

ME477
Fall 2005
Solution for Homework #5

Chapter 26: Multiple Choice Questions

26.5 (c) and (d)

26.7 (e)

26.10 (d)

Problems

26.5**Solution:** (a) From Table 26.1, $C = 0.000126 \text{ in}^3/\text{A-min}$.

$$\text{MRR} = f_r \times A = (CI/A)(A) = CI$$

$$\text{MRR} = CI = 0.000126(1500) = 0.189 \text{ in}^3/\text{min} \text{ at } 100\% \text{ efficiency.}$$

At 90% efficiency $\text{MRR} = 0.189(0.90) = 0.1701 \text{ in}^3/\text{min} = \mathbf{10.206 \text{ in}^3/\text{hr}}$.

(b) $I = EA/gr$; Rearranging, $g = EA/Ir = 12(2.5)/(1500 \times 6.2) = \mathbf{0.0032 \text{ in}}$.

26.11**Solution:** From Table 4.1, $T_m = 2802^\circ\text{F}$ for iron.

$$\text{MRR} = 5.08 I/2802^{1.23} = 5.08 I/17,393 = 0.000292 I \text{ in}^3/\text{min}$$

Given that $\text{MRR} = 0.01 \text{ in}^3/\text{min}$.

$$0.000292 I = 0.01$$

$$I = 0.01/0.000292 = 34.24 \text{ A.}$$

From Table 4.1, $T_m = 2651 \text{ F}$ for iron.

$$\text{MRR} = 5.08(34.24)/2651^{1.23} = 173.93/16,248 = \mathbf{0.0107 \text{ in}^3/\text{min}}$$

26.16**Solution:** (a) Neglecting the fact that the initial area would be less than the given dimensions of 9

in. by 6 in., and that the material removal rate (MRR) would therefore increase during the cut as

the area increased, area of an ellipse $A = \pi ab = \pi(9.0)(6.0) = 54\pi = 169.65 \text{ in}^2$

$$\text{MRR} = (0.001 \text{ in}/\text{min})(169.65 \text{ in}^2) = 0.16965 \text{ in}^3/\text{min} = \mathbf{10.18 \text{ in}^3/\text{hr}}$$

(b) Time to machine (etch) = $0.4/0.001 = \mathbf{400 \text{ min.}} = \mathbf{6.67 \text{ hr}}$.

(c) Given $F_e = 2.0$, undercut $u = d/F_e = 0.4/2.0 = 0.2 \text{ mm}$

Maskant opening $a' = a - u = 9.0 - 0.2 = \mathbf{8.8 \text{ in}}$

Maskant opening $b' = b - u = 6.0 - 0.2 = \mathbf{5.8 \text{ in}}$

Chapter 28: Multiple Choice Questions

28.1(a), (c), (d), and (e).

28.5(a), (b), (c), (d), and (e).

28.6(a)

Chapter 29: Multiple Choice Questions ()

29.4 either (a) or (b) is acceptable

29.7(e)

29.11(b) and (c).

29.14(a)

Problems

29.3**Solution:** From Table 29.1, $C = 0.92 \times 10^{-4} \text{ in}^3/\text{A-min}$, cathode efficiency $E = 15\%$.

Volume $V = ECIt = 0.15(0.92 \times 10^{-4})(15)(10) = 0.00207 \text{ in}^3$.

Plating thickness $d = 0.00207/15 = \mathbf{0.000138 \text{ in}}$.

29.6**Solution:** From Table 29.1, $C = 2.69 \times 10^{-4} \text{ in}^3/\text{A-min}$, cathode efficiency $E = 98\%$.

Required volume of plate metal $= 36(0.001) = 0.036 \text{ in}^3$

Plated volume $V = ECIt = 0.98(2.69 \times 10^{-4} \text{ in}^3/\text{A-min})(15 \text{ A}) t = 0.003954 t \text{ in}^3$.

$0.003954 t = 0.036 t = 0.036/0.003954 = \mathbf{9.1 \text{ min}}$.

Chapter 30: Multiple Choice Questions

30.6(b)

30.7(b) and (c)

Problems

30.3**Solution:** (a) Area $A = \pi(0.1)^2/4 = 0.00785 \text{ in}^2$

$150 \text{ Btu/min} = 2.5 \text{ Btu/sec}$.

Power $P = 0.50(2.5) = 1.25 \text{ Btu/sec}$

Power density $PD = (1.25 \text{ Btu/sec})/0.00785 \text{ in}^2 = \mathbf{159 \text{ Btu/sec-in}^2}$

(b) $A = \pi(0.25^2 - 0.1^2)/4 = 0.0412 \text{ in}^2$

Power $P = (0.75 - 0.50)(2.5) = 0.625 \text{ Btu/sec}$

Power density $PD = (0.625 \text{ Btu/sec})/0.0412 \text{ in}^2 = \mathbf{15.16 \text{ Btu/sec-in}^2}$

(c) Power densities are sufficient certainly in the inner circle and probably in the outer ring for welding.

30.8**Solution:** (a) Eq. (30.2) for SI units: $U_m = 3.33 \times 10^{-6} T_m^2$

From Table 30.2, T_m for austenitic stainless steel $= 1670 \text{ K}$

$U_m = 3.33 \times 10^{-6} (1670)^2 = 9.29 \text{ J/mm}^3$

Volume of metal melted $V = 20(200) = 4000 \text{ mm}^3$

$H_m = 9.29(4000) = \mathbf{37,148 \text{ J}}$ at weld

(b) Given $f_1 = 0.8$ and $f_2 = 0.6$. $H = 37,148/(0.8 \times 0.6) = \mathbf{77,392 \text{ J}}$ at source.

30.15**Solution:** $U_m = 1.467 \times 10^{-5} (1800 + 460)^2 = 74.9 \text{ Btu/in}^3$

$v = f_1 f_2 HR/U_m A_w = 0.8(0.5)(125)/(74.9 \times 0.04) = \mathbf{16.7 \text{ in/min}}$.

Chapter 31: Multiple Choice Questions

31.6(b) The arc is sustained, not by the transfer of molten metal, but by the presence of a thermally ionized column of gas through which the current flows.

31.10(a)

31.17(a) and (b)

Problems

31.3**Solution:** (a) $HR_w = f_1 f_2 EI = (0.85)(0.75)(30)(225) = \mathbf{4303.1 \text{ W}}$

(b) $WVR = (4303.1 \text{ W})/(10.2 \text{ J/mm}^3) = \mathbf{421.9 \text{ mm}^3/\text{sec}}$.

31.10**Solution:** (a) $PD = I_2R/A$

$$A = \pi D^2/4 = \pi(0.19)^2/4 = 0.02835 \text{ in}^2$$

$$I_2R = (9500)^2(100 \times 10^{-6}) = 9025 \text{ W}$$

$$1 \text{ Btu/sec} = 1055 \text{ W, so } 9025 \text{ W} = 8.554 \text{ Btu/sec}$$

$$PD = 8.554/0.02835 = \mathbf{302 \text{ Btu/sec-in}^2}$$

$$(b) H = I_2Rt = (9500)^2(100 \times 10^{-6})(0.17) = 1534 \text{ W-sec} = 1.454 \text{ Btu}$$

$$\text{Weld nugget volume } V = \pi D^2d/4 = \pi(0.19)^2(0.060)/4 = 0.0017 \text{ in}^3$$

$$\text{Heat required for melting} = U_mV = (150 \text{ Btu/in}^3)(0.0017) = 0.255 \text{ Btu}$$

$$\text{Proportion of heat for welding} = 0.255/1.454 = \mathbf{0.175 = 17.5\%}$$

31.17**Solution:** Available heat for welding $HR_w = f_1f_2EI = U_mA_wv$

$$\text{Travel velocity } v = f_1f_2EI/U_mA_w$$

$$\text{Cross sectional area of weld seam } A_w = (0.35)(3.0) = 1.05 \text{ mm}^2$$

$$v = 0.85(0.75)(25 \times 10^3)(30 \times 10^{-3})/(5.0 \times 1.05) = \mathbf{91.05 \text{ mm/s}}$$

Chapter 32: Multiple Choice Questions

32.2(b)

32.4(b)

32.9(a), (c), (d), and (e)

32.13(c) and (d)

Chapter 33: Multiple Choice Questions

33.4(b), (c), and (d)

33.9(a) and (e)

Problems

$$33.5\mathbf{Solution:} F = T/CD = 125/(0.2 \times 0.75) = 833.3 \text{ lb.}$$

$$A_s = 0.25\pi(0.75 - 0.9743/10)^2 = 0.334 \text{ in}^2$$

$$\sigma = 833.3/0.334 = \mathbf{2495 \text{ lb/in}^2}$$

Chapter 34: Multiple Choice Questions

34.4(a), (e), and (f)

34.8(b), (c), and (d)

Problems

34.1**Solution:** Layer area A_i same for all layers.

$$A_i = 100^2 - 90^2 = 1900 \text{ mm}^2$$

Time to complete one layer T_i same for all layers.

$$T_i = (1900 \text{ mm}^2)/(0.25 \text{ mm})(500 \text{ mm/s}) + 10 \text{ s} = 15.2 + 10 = 25.2 \text{ s}$$

$$\text{Number of layers } n_i = (80 \text{ mm})/(0.10 \text{ mm/layer}) = 800 \text{ layers}$$

$$T_c = 800(25.2) = \mathbf{20,160 \text{ s} = 336.0 \text{ min} = 5.6 \text{ hr}}$$

Chapter 35: Multiple Choice Questions

35.3(d)

35.5(b)

35.8(c)

35.10(a)

Problems

35.1 Solution: (a) Total volume $V = V_1$ (tang) + V_2 (cylinder) + V_3 (seed)

$$V_1 = V_3 = (\text{cone in which } h = 0.5(1200-950) = 125, D = 110, R = 55) = \pi R^2 h / 3 \\ = 0.333\pi(55)^2(125) = 395,972 \text{ mm}^3.$$

$$V_2 = \pi R^2 L = \pi(55)^2(950) = 9,028,152 \text{ mm}^3$$

$$\text{Total } V = 2(395,972) + 9,028,152 = \mathbf{9,820,095 \text{ mm}^3}$$

(b) Number of wafers = $950 / (0.50 + 0.33) = 1144.6 \rightarrow \mathbf{1144 \text{ wafers}}$

(c) Area of one wafer $A_w = A_c - A_s$, where A_c = area of the circle of radius $R = 50$ mm, and A_s = the area of the segment A_s created by the flat ground on the cylindrical surface.

$$A_c = \pi R^2 = \pi(50)^2 = 7854.0 \text{ mm}^2$$

The area of a segment of the circle created by the 30 mm chord $A_s = \pi R^2 \theta / 360 - 0.5 R^2 \sin \theta$, where θ is the angle formed by two radii of the circle and the chord. $.50 = \sin^{-1}(15/50) = 17.46^\circ$.

$$\theta = 34.92^\circ.$$

$$A_s = \pi(50)^2(34.92)/360 - 0.5(50)^2 \sin 34.92 = 761.8 - 715.5 = 46.3 \text{ mm}^2$$

$$A_w = A_c - A_s = 7854.0 - 46.3 = 7807.7 \text{ mm}^2$$

$$\text{Volume of one wafer } V_w = A_w t = 7807.7(0.5) = 3903.8 \text{ mm}^3$$

$$\text{Volume of 1144 wafers} = 1144(3903.8) = 4,465,994 \text{ mm}^3$$

$$\text{Volume wasted} = 9,820,095 - 4,465,994 = 5,354,101 \text{ mm}^3$$

$$\text{Proportion wasted} = 5,354,101 / 9,820,095 = \mathbf{54.52\%}.$$

35.14 Solution: (a) Rent's rule: $n_{io} = 6.0 n_c$

$$0.12 = 6.0 (64 \times 64)^{0.12} = 6.0(4096)^{0.12} = 16.3 \rightarrow \mathbf{16 \text{ pins}}$$

$$(b) \text{ Eq. (35.11): } n_{io} = 1.4427 \ln (64 \times 64) = 1.4427 \ln 4096 = \mathbf{12 \text{ pins.}}$$

Chapter 36: Multiple Choice Questions

36.2(c)

36.6(a)

36.10(a)