

Mathematical singularities associated with swelling of hyperelastic solids

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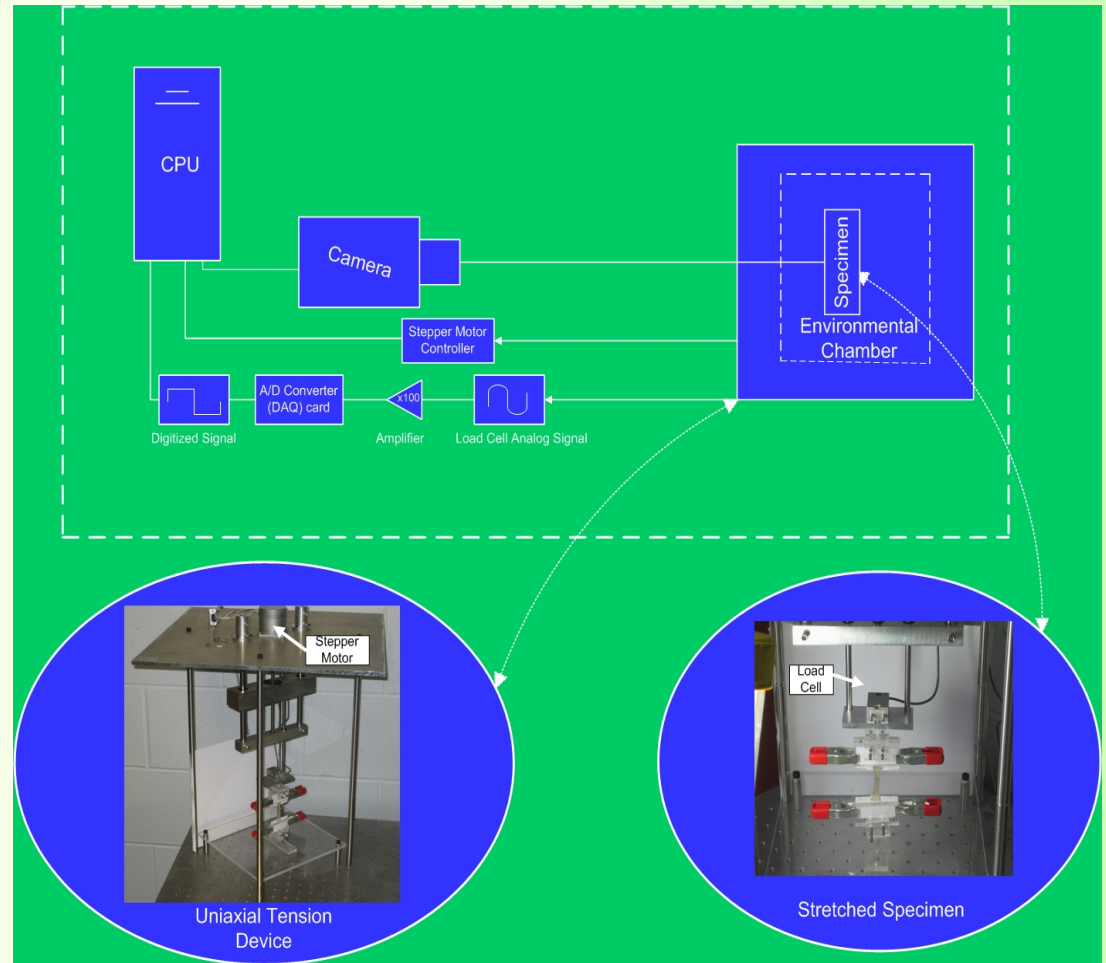
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Swelling occurs in a variety of soft materials: rubbers and polymers, elastomer gels, soft materials.



source www.math.utah.edu/~hsu/presentations/IGERT_pres by Prof. V. Hsu

“swelling” google hits: 17,300,00,

“swelling remedies” google hits: 1,500,000

A variety of mathematical treatments and traditions

- Poroelasticity with Darcy’s law and Fick’s law,
- Large deformation mechanics of mixtures theory (interacting media),
- Solid mechanics with energy densities that depend on a variable natural free volume.

Solid mechanics with energy densities that depend on a variable natural free volume is a simple generalization of the **standard hyperelastic framework**.

$\mathbf{y} = \mathbf{y}(\mathbf{X})$ maps reference configuration to deformed configuration,

with deformation gradient $\mathbf{F} = \frac{\partial \mathbf{y}}{\partial \mathbf{X}}$

volume change $J = \det \mathbf{F}$, if incompressible then $J = 1$

Elastic stored energy density $W=W(\mathbf{F}, \mathbf{X}, \underline{E})$ where \underline{E} denotes a list of any constitutive parameters, e.g., stiffness moduli (convexity of wells).

Cauchy stress: $\sigma = \frac{1}{J} \frac{\partial W}{\partial \mathbf{F}} \mathbf{F}^T$, for compressible materials,

$\sigma = \frac{1}{J} \frac{\partial W}{\partial \mathbf{F}} \mathbf{F}^T - p \mathbf{I}$, for incompressible materials.

The stress equations of equilibrium $\operatorname{div} \boldsymbol{\sigma} = \mathbf{0}$ are then Euler-Lagrange equations for minimizing the total stored elastic energy.

Simple generalization to treat swelling is to introduce the natural free volume as a variable

$v = \text{natural free volume}$, dependent on temperature, chemical environment, stress, etc.

such that now $W = W(\mathbf{F}, \mathbf{X}, \underline{E}, v)$ and the usual minimization again gives $\text{div} \boldsymbol{\sigma} = \mathbf{0}$.

If the material is **compressible** after swelling, then
$$\boldsymbol{\sigma} = \frac{1}{J} \frac{\partial W}{\partial \mathbf{F}} \mathbf{F}^T,$$

If the material is **incompressible** after swelling, then

$$\boldsymbol{\sigma} = \frac{1}{v} \frac{\partial W}{\partial \mathbf{F}} \mathbf{F}^T - p \mathbf{I}, \quad \text{subject to } J = v.$$

In addition to the usual “loading” due to tractions and body forces, there is the possibility of additional loading due to:

- confinement that gives rise to internal stress when swelling occurs,
- nonuniform swelling $v = v(\mathbf{X})$ in which case $\text{div} \boldsymbol{\sigma} = \mathbf{0}$ involves a “configurational force term”.

Dependence of W upon v

If $W(\mathbf{F}, \mathbf{X}, \underline{E})$ is a ``conventional'' hyperelastic energy density in that it registers an appropriate energy well structure for fixed free volume, then $W(v^{-1/3} \mathbf{F}, \mathbf{X}, \underline{E}(v))$:

- shifts energy wells in keeping with the notion of an energy minimal free volume by virtue of $v^{-1/3} \mathbf{F}$,
- allows for swelling dependent modulus changes by virtue of $\underline{E}(v)$.

Modulus parameters that grow slower than $O(v)$ give rise to modulus softening (as observed in gels) when mechanical response is linearized about the swollen state.

Example: conventional material (Shang-Cheng):

$$W = \frac{\mu}{2} \left(\lambda_1 + \lambda_2 + \lambda_3 + 3 \left(\frac{1}{\lambda_1} + \frac{1}{\lambda_2} + \frac{1}{\lambda_3} \right) + 2\lambda_1\lambda_2\lambda_3 - 14 \right)$$

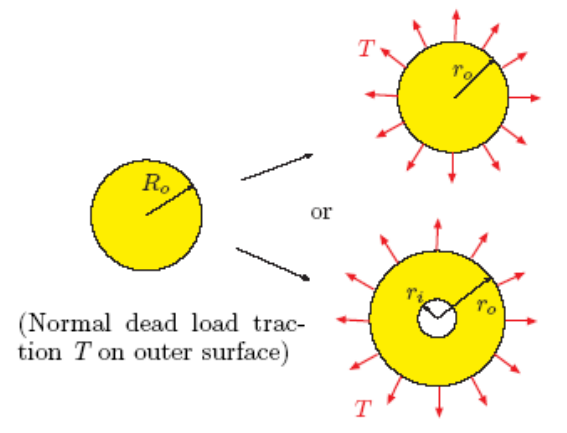
with swelling:

$$W = \frac{\mu v^q}{2} \left(\frac{\lambda_1}{v^{1/3}} + \frac{\lambda_2}{v^{1/3}} + \frac{\lambda_3}{v^{1/3}} + 3 \left(\frac{v^{1/3}}{\lambda_1} + \frac{v^{1/3}}{\lambda_2} + \frac{v^{1/3}}{\lambda_3} \right) + \frac{2}{v} \lambda_1\lambda_2\lambda_3 - 14 \right)$$

$$(0 < q < 1)$$

Cavitation

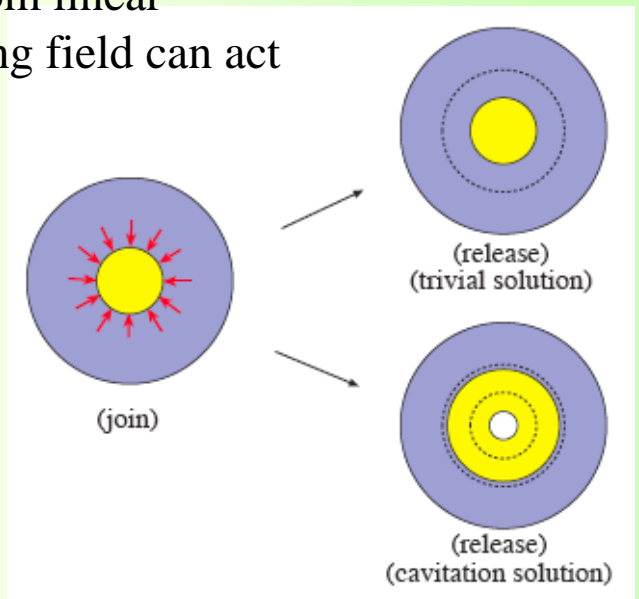
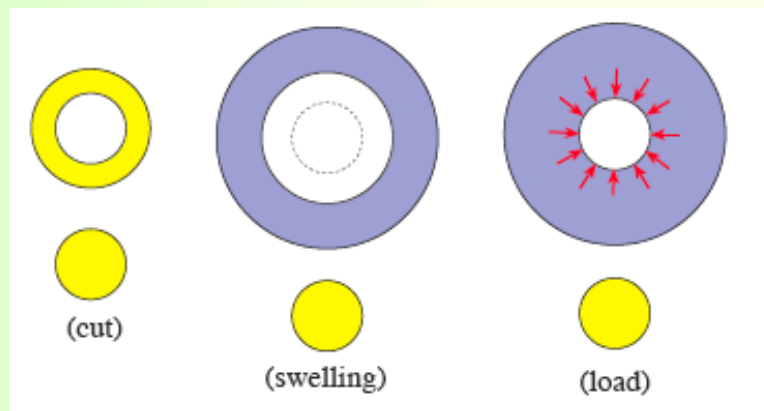
For swelling induced cavitation, consider a piecewise constant swelling field, where an outer layer swells while the inner core does not.



$$v = 1, \quad 0 \leq R < R_m$$

$$v = \bar{v} > 1, \quad R_m < R \leq R_o$$

A “cut, swell, load, join, release” argument (familiar from linear eigenstrain/inclusion analysis) suggests how this swelling field can act as an effective loading device.



Spherical geometry: principal stretches are

$$\beta = \frac{dr}{dR}, \quad \lambda = \frac{r}{R}.$$

with $\mathbf{F} = \beta \mathbf{e}_r \otimes \mathbf{e}_R + \lambda(\mathbf{e}_\theta \otimes \mathbf{e}_\Theta + \mathbf{e}_\phi \otimes \mathbf{e}_\Phi)$

$$\beta_i := \beta \Big|_{R \rightarrow 0^+}, \quad \beta_m^- := \beta \Big|_{R \rightarrow R_m^-}, \quad \beta_m^+ := \beta \Big|_{R \rightarrow R_m^+}, \quad \beta_o := \beta \Big|_{R=R_o},$$

$$\lambda_i := \lambda \Big|_{R \rightarrow 0^+}, \quad \lambda_m := \lambda \Big|_{R=R_m}$$

$$\lambda_o := \lambda \Big|_{R=R_o}$$

The ODE associated with radial equilibrium admits a variety of solution alternatives:

- a conventionally smooth solution with no cavitation.
- a cavitation solution. (Preceded by a smooth solution with $\lambda_i \rightarrow \infty$)
- no smooth solutions capable of satisfying interfacial BC of λ continuity. (Preceded by a smooth solution with $\beta_m^+ \rightarrow \infty$)

Example: A swellable compressible surface layer over an incompressible core material that supports cavitation.

Layer $R_m \leq R \leq R_o$ is a compressible Shang-Cheng swelling material with $q = 1/3$,

Core $0 \leq R \leq R_m$ is an incompressible Varga material:

$$W_{core}(\lambda_1, \lambda_2, \lambda_3) = 2\mu_{core}(\lambda_1 + \lambda_2 + \lambda_3 - 3)$$

Smooth solutions exist provided the swelling is not too large

For given R_m and R_o let $\xi = R_m/R_o$ so that $0 \leq \xi \leq 1$. Then there exists $V_{max} = V_{max}(\xi)$ such that there is a unique smooth radially symmetric solution for $1 \leq \bar{v} < V_{max}(\xi)$ while there are no such smooth solutions for $\bar{v} \geq V_{max}(\xi)$.

As $\bar{v} \rightarrow V_{max}(\xi)$ one finds that $\beta_m^+ \rightarrow \infty$

Cavitation solutions are possible only if the core is sufficiently soft, whereupon such solutions exist if the swelling is sufficiently large.

$$\mu_{core} < \left(\frac{1}{4} + \frac{1}{2}V_{max}^{-2/3}\right)\mu$$

$$\bar{v} > V_{nuc} = V_{nuc}(\xi, \mu_{core}/\mu)$$

Thank You

Questions?

