

Please start with an easy question and try to answer all questions.

Problem:	1	2	Total
Max. Grade:	30	80	100+10(extra)
Grade:	30	80	110

great!

1 Problem

Consider the second order system

$$G(s) = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}$$

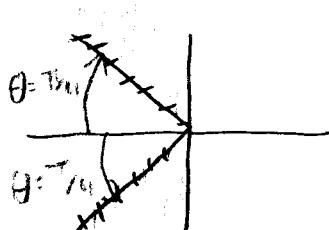
and the following two performance specifications:

1. $G(s)$ is stable,
2. Percent Overshoot (PO) $> 4.3\%$, and
3. 5% settling time < 3 sec.

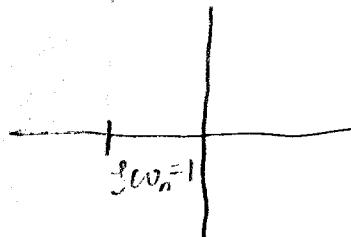
Provide answers to the following questions.

- a. (10 points) Find (or draw) all possible locations of the two poles of $G(s)$ in the complex domain to satisfy stability and PO conditions.
- b. (10 points) Find all possible locations of the two poles of $G(s)$ in the complex domain to satisfy the settling time condition.

a) $PO > 4.3\%$
 $\Rightarrow \theta > \theta_m = 71^\circ$



b) $5\% \text{ settling time} < 3 \text{ sec}$
 $t_s < t_{sm}$
 $\Im \omega_n > \frac{3}{t_{sm}} = \frac{3}{3} = 1$



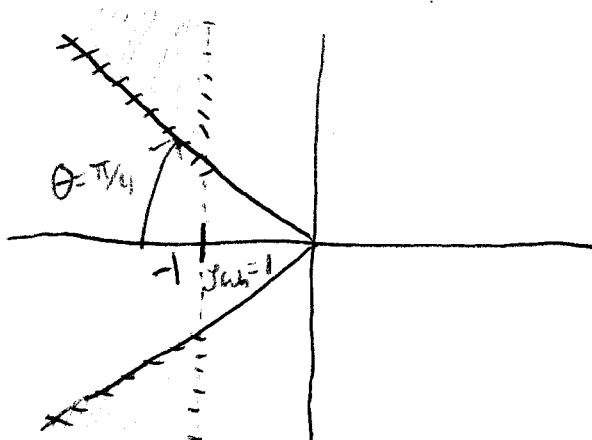
- c. (10 points) Find all possible locations of the two poles of $G(s)$ in the complex domain to satisfy stability, PO and settling time conditions.

Hint:

$$PO = 100e^{\frac{-\zeta\pi}{\sqrt{1-\zeta^2}}} = 100e^{-\pi/\tan\theta},$$

where $\zeta = \cos\theta$. From this equation, we know that $\theta = \pi/4$ when $PO = 4.3\%$.

c) $PO > 4.3\% \Rightarrow \theta > \theta_m = \pi/4$



5% settling time
 $t_s < 3 \text{ sec}$
 $\Rightarrow \Im\omega_n > \frac{3}{t_{sm}} = \frac{3}{3}$

2 Problem

Consider the transfer function

$$G(s) = \frac{s+1}{(s^2 + 2^2)(s+3)}$$

in the feedback system in Fig. 1.

- a. (5 points) What is the root locus? Explain by using Fig. 1.
- b. (15 points) Draw the root locus by varying k from 0 to ∞ . What is the relative degree? Show the intersection of asymptotes.
- c. (10 points) Find the range of $k > 0$ for which the closed-loop system is stable.
- d. (10 extra points) Compute the angle of departures for the complex poles of the open-loop transfer function.
- e. (15 points) For a unit step input $U(S) = \frac{1}{s}$, compute the steady state error $e_{ss} := \lim_{t \rightarrow \infty} [e(t) := u(t) - y(t)]$ in terms of k .
- f. (15 points) Propose a dynamical controller (in stead of using a constant gain k) in order to eliminate the steady state error for the unit step input completely. Justify your answer.
- g. (10 points) Explain how you prove the stability of the closed-loop system with the dynamical controller you provided.

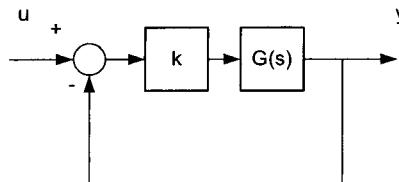
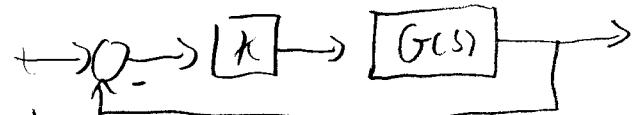


Figure 1: A closed-loop system.

- a) The root locus is a visual representation of the possible pole locations in Figure 1, assuming the constant K is in the range $0 < K < \infty$. This can also tell you the natural frequency, damping ratio, and damping frequency of the system for a given K as well as the stability. \rightarrow

b)

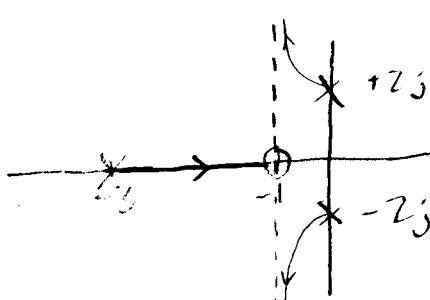


$$G(s) = \frac{s+1}{(s^2+2^2)(s+3)}$$

Assume stable CL transfer function (poles in left half plane)

Zeros: -1

Poles: $\pm j\omega_0, -3$



relative degree

$$\text{r} = \text{degree(den)} - \text{degree(num)} \\ = 3 - 1 = 2$$

$$\text{Intersection} = \frac{\sum \text{Poles} - \sum \text{Zeros}}{\text{r}} \\ = \frac{(+j\omega_0 - j\omega_0 - 3) - (-1)}{2} \\ = \frac{-2}{2} = -1$$

C) Characteristic eq of closed loop

$$(s^2 + 4)(s+3) + K(s+1) = 0$$

$$s^3 + 3s^2 + (4+K)s + 12 + K = 0$$

Routh Array

$$\begin{aligned} & \frac{(4+K) - (12+K)}{3} \\ &= \frac{3}{4+K} - \frac{4+K}{3} \\ &= \frac{2}{3}K \end{aligned}$$

s^3	1	$4+K$
s^2	3	$12+K$
s^1	$\frac{2}{3}K$	
s^0	$12+K$	

For a stable system:

$$-12 < K$$

$$+0 < K$$

$$-12 < 0 \therefore K > 0$$



$$d) \quad L(s) = \frac{s+1}{(s+4)(s+3)} = \frac{s+1}{(s+z_j)(s-z_j)(s+3)}$$

$$\lim_{S_0 \rightarrow P_1} \angle L_{ss} = \angle (S_0 - Z_1) - \angle (S_0 - P_1) - \angle (S_0 - P_2) \\ \sim - \angle (S_0 - P_3) = 180^\circ$$

θ_{dep}

$$\angle (S_0 - P_1) = \angle (P_1 - Z_1) - \angle (P_1 - P_2) - \angle (P_1 - P_3) + 180^\circ$$

$$P_1 - Z_1 = 2j - (-1) = 1 + Z_j$$

$$\angle (P_1 - Z_1) = \tan^{-1}(3) = 63.43^\circ$$

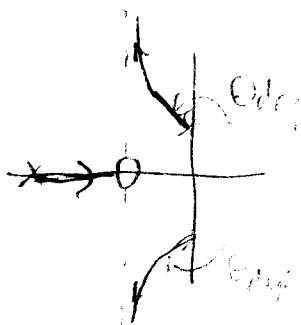
$$P_1 - P_2 = 2j - (-2j) = 4j$$

$$\angle (P_1 - P_2) = 90^\circ$$

$$P_1 - P_3 = 2j - (-3) = 3 + Z_j$$

$$\angle (P_1 - P_3) = \tan^{-1}(3) = 33.69^\circ$$

$$\theta_{dep} = 63.43^\circ - 90^\circ - 33.69^\circ + 180^\circ \\ = 119.741^\circ$$



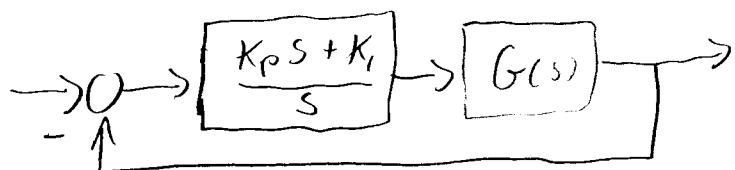
e) Let it is a unit step
 $U(s) = \frac{1}{s}$

$$e_{ss} = \frac{1}{1 + K_p} = \frac{1}{1 + K/12}$$

$$\begin{aligned} K_p &= \lim_{s \rightarrow 0} G(s) \\ &= K \left(\frac{0+1}{(0^2+1)(0+3)} \right) = \frac{K}{12} \end{aligned}$$

f) I would suggest adding a PI controller. This would increase the system's type from a 0 to a 1.

$$PI = \frac{K_p s + K_i}{s}$$



Open loop transfer function becomes $\frac{()}{s()}$

$$\begin{aligned} e_{ss} &= \frac{1}{1 + K_p} ; \text{ where } K_p = \lim_{s \rightarrow 0} G(s) \\ &= \frac{1}{1 + \frac{K}{12}} = \frac{12}{13} \end{aligned}$$

$$e_{ss} = \frac{1}{1 + \infty} = 0$$

g) The stability can be proved either by substituting the root characteristic eq into the Routh array or by drawing the root locus.

If the root locus is ^{only} in the left half plane the system is stable.

If the first column of the Routh array does not change signs the system is stable.

s^4	1	0	0	0
s^3	0	-1	0	0
s^2	0	0	-1	0
s^1	0	1	0	0
s^0	1	0	0	0