

MICHIGAN STATE UNIVERSITY
 Department of Mechanical Engineering
 ME451 Control Systems Spring 2007
Midterm Exam II

Closed Book. Two 8.5 × 11 pages of handwritten notes are allowed.

Your Name:	Solution
Student Number:	

Please answer all questions.

Problem:	1	2	Total
Max. Grade:	50	50	100
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1 Problem

a. (20 points) Determine the range of the controller gains (K, K_I) so that the PI feedback system in Fig. 1 is BIBO (or asymptotically) stable. Plot this range in a two-dimensional space. (Hint: Use the Routh-Hurwitz stability test.)

$e_{ss} = \frac{3}{4}$

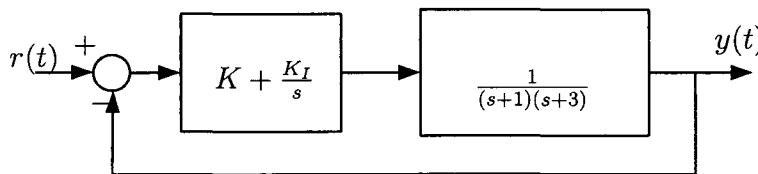
b. (10 points) Set gains at $K = 1, K_I = 0$. Consider a unit step input $R(s) = \frac{1}{s}$. Determine the steady state error $e_{ss} := \lim_{t \rightarrow \infty} e(t)$, where $e(t) := r(t) - y(t)$.

$e_{ss} = 0$

c. (10 points) Set gains at $K = 1, K_I = 0.01$. Consider a unit step input $R(s) = \frac{1}{s}$. Determine the steady state error $e_{ss} := \lim_{t \rightarrow \infty} e(t)$, where $e(t) := r(t) - y(t)$.

d. (10 points) Set gains at $K = 1, K_I = 0$. Consider a sinusoidal input signal $r(t) = 10 \sin(2t)$. Determine the steady state signal $y_{ss}(t)$ for this input.

$y_{ss}(t) = \frac{10}{8} \sin(2t - \frac{\pi}{2})$



Check the location of closed-loop poles

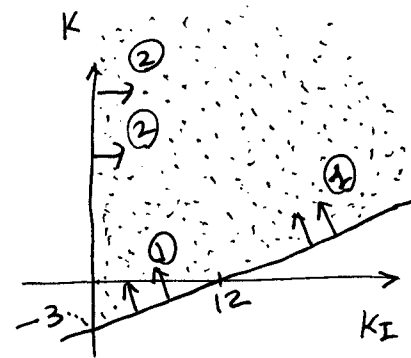


Figure 1: A system with a PI controller.

(a) C.E. $\Rightarrow 1 + (K + \frac{K_I}{s}) \frac{1}{(s+1)(s+3)} = 0$

or $1 + \frac{sK + K_I}{s} \frac{1}{(s+1)(s+3)} = 0$

$\rightarrow s(s^2 + 4s + 3) + sK + K_I = 0$

C.E. $s^3 + 4s^2 + (3+K)s + K_I = 0$

Routh-Array

s^3	1	$3+K$
s^2	4	K_I
s^1	b	
s^0	$K_I > 0$	— ②

$b = -\frac{1}{4} \left| \begin{array}{cc} 1 & 3+K \\ 4 & K_I \end{array} \right| = -\frac{1}{4} (K_I - 12 - 4K) > 0$ — ①
 \rightarrow or $K_I - 12 - 4K < 0$

} Stability Condition

TF from r to e

b.
$$T_{r \rightarrow e} = \frac{1}{1 + \left(K + \frac{K_I}{s}\right) \frac{1}{(s+1)(s+3)}}$$

$$E(s) = R(s) \cdot T_{r \rightarrow e}(s)$$

(K=1, K_I=0) ⇒ system is stable by ①, ②

use Final value theorem

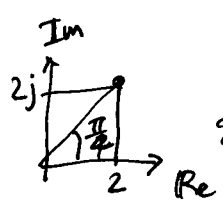
$$e_{ss} = \lim_{s \rightarrow 0} s E(s) = \lim_{s \rightarrow 0} s \cdot \frac{1}{1 + (1) \cdot \frac{1}{(s+1)(s+3)}} = \frac{1}{1 + \frac{1}{3}} = \boxed{\frac{3}{4}}$$

c. (K=1, K_I=0.01) system is stable by ①, ② use F.V.T.

$$e_{ss} = \lim_{s \rightarrow 0} s E(s) = \lim_{s \rightarrow 0} s \cdot \frac{1}{1 + \left(1 + \frac{0.01}{s}\right) \frac{1}{(s+1)(s+3)}} = \frac{1}{\infty} = \boxed{0}$$

d.

T.F. from r to y
$$T_{r \rightarrow y}(s) = \frac{F_y}{1 - L_y} = \frac{1}{(s+1)(s+3)} \cdot \frac{1}{1 + \frac{1}{(s+1)(s+3)}} = \frac{1}{s^2 + 4s + 4} = \frac{1}{(s+2)^2}$$



$$T_{r \rightarrow y}(j2) = \frac{1}{(2j+2)^2} = \frac{1}{(2\sqrt{2} e^{\frac{\pi}{4}j})^2} = \frac{1}{4 \cdot 2} e^{-\frac{\pi}{2}j}$$

↑ magnitude ↑ phase

$$y_{ss}(t) = 10 \cdot \left(\frac{1}{4 \cdot 2}\right) \cdot \sin\left(2t - \frac{\pi}{2}\right)$$

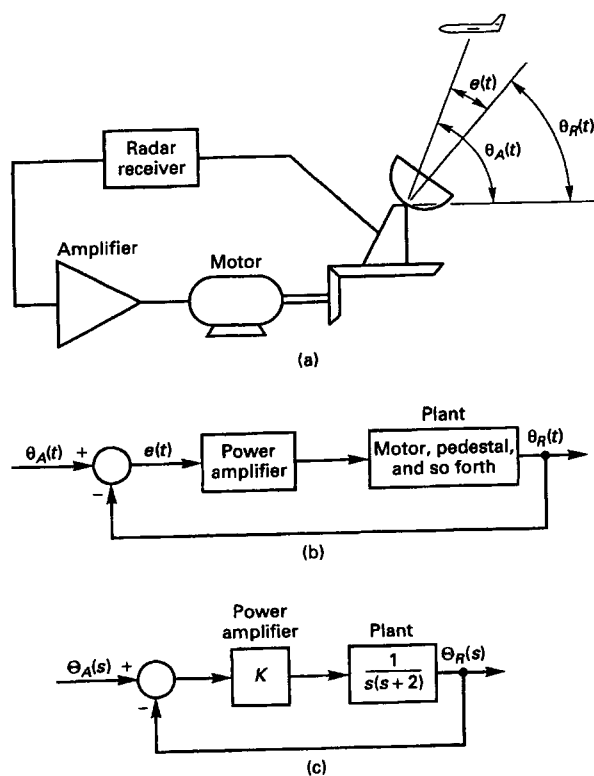


Figure 2: Radar Tracking System.

2 Problem

Consider the radar tracking system illustrated in Fig. 2. We need to design the tracking system so that the radar tracks the target airplane properly, i.e., $\theta_R(t)$ should be able to track $\theta_A(t)$ properly.

- Handwritten:* $1 \leq K \leq 2$
- (15 points) Draw the root locus of the system. Specify the location of a break away point. (Hint: Obtain the closed loop poles in terms of K . Plot them as you vary K from 0 to ∞ in s -plane.)
 - (20 points) An airforce Colonel demands the following time specifications of the closed-loop second order system with a step input $\theta_A(t)$:
 - Spec. 1* • the system has to be either critically damped or underdamped for fast dynamics,
 - Spec. 2* • the maximum allowable settling time T_s is 4 sec. (Hint: use $T_s = \frac{4}{\zeta\omega_n}$.),
 - Spec. 3* • the maximum allowable percentage overshoot is 4.32 %. (Hint: this is achieved by $\zeta = 0.707$.)

Determine the range of K for which the closed-loop system satisfies the time specifications.

- Handwritten:* $e_{th} = 1$
- (15 points) Fix $K = 2$. For a unit ramp input $\Theta_A(s) = \frac{1}{s^2}$, determine the steady state error $e_{ss} := \lim_{t \rightarrow \infty} e(t)$, where $e(t) = \theta_A(t) - \theta_R(t)$ as shown in Fig. 2-(b).

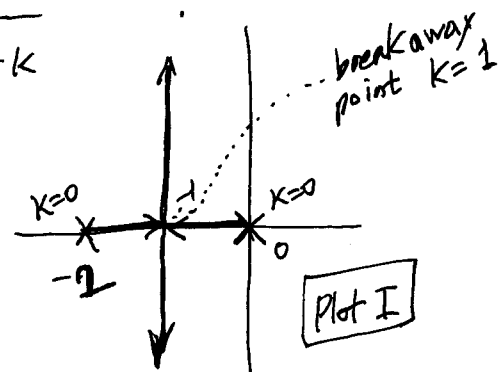
T.F. From θ_A to θ_R

(a)

$$T(s) = \frac{K \frac{1}{s(s+2)}}{1 + K \frac{1}{s(s+2)}} = \frac{K}{s^2 + 2s + K}$$

C.E. $s^2 + 2s + K = 0$

$$s_{1,2} = -1 \pm \sqrt{1-K}$$



- $0 \leq K < 1 \rightarrow$ overdamped system \times with spec. 1 ($s_{1,2} = -1 \pm \sqrt{1-K}$)
- $K = 1 \rightarrow$ critically damped system (two roots at -1)
- $1 < K < \infty \rightarrow$ under damped system ($s_{1,2} = -1 \pm \sqrt{K-1}j$)

(b)

From Spec 1. $\rightarrow K \geq 1$

From Spec 2. $\rightarrow T_s = \frac{4}{\zeta \omega_n} \leq 4 \rightarrow -\zeta \omega_n \leq -1$

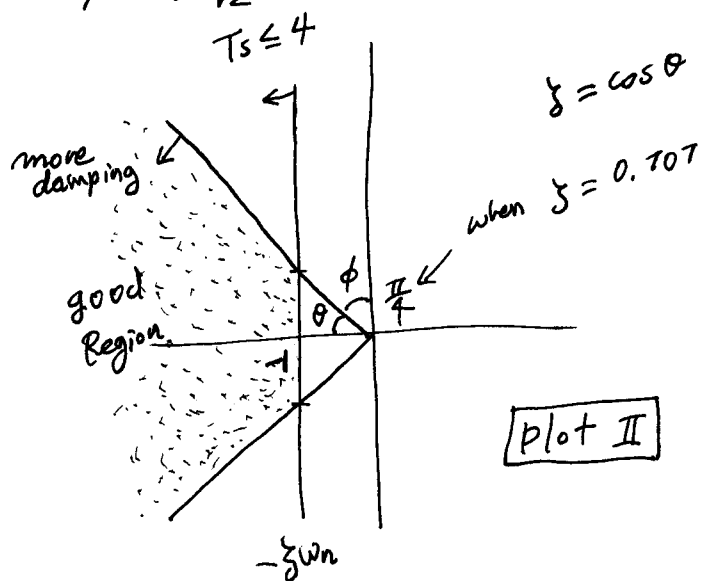
From Spec 3. $\rightarrow \zeta = \cos \theta = \sin \phi \geq \frac{1}{\sqrt{2}}$

Range of K satisfies spec 1.-3.

$$1 \leq K \leq 2$$

when $K = 2$

$$s_{1,2} = -1 \pm j$$



(c)

$$T_{\text{type}} = \frac{1}{1 + K \frac{1}{s(s+2)}}$$

$K = 2 \rightarrow$ stable

$$e_{ss} = \lim_{s \rightarrow 0} s E(s) = \lim_{s \rightarrow 0} s \cdot \frac{1}{s^2} \left[\frac{1}{1 + \frac{2}{s(s+2)}} \right] = \lim_{s \rightarrow 0} \frac{1}{s + \frac{2}{(s+2)}} = 1$$