

# ME 201

## Thermodynamics

### Exam #2 Solution

#### Problem 1

Steam at 300 kPa with quality 0.96316 passes through a valve to convert it to saturated vapor. Determine the exit pressure required.

**Solution:** We begin with our template.

Substance Type: Compressible

System Type: Control Volume

Device: Valve

Process: Isenthalpic

Inlet State: Fixed

Outlet State: UNKNOWN

$$q = 0$$

$$w_{sh} = 0$$

$$\text{1st Law: } h_2 - h_1 = 0$$

<u>State 1</u>	<u>State 2</u>
$T_1 = 133.52^\circ\text{C}$	$T_2 = 81.31^\circ\text{C}$
$P_1 = 300 \text{ kPa}$	$P_2 = 50 \text{ kPa}$
$h_1 = 2645.2 \text{ kJ/kg}$	$h_2 = \mathbf{2645.2 \text{ kJ/kg}}$
Phase: 2 phase with $x_1 = 0.96316$	Phase: sat.vap

*Italicized* values are from steam tables. **Bold** values are calculated.

Approach: Go to the steam tables and get  $h_f$  and  $h_g$  at 300 kPa. Use the quality to calculate  $h_1$ . Set  $h_2 = h_1$ . Go to the saturation pressure table and find the pressure that gives an  $h_g = h_2$ .

At 300 kPa, we have

$$h_f = 561.43 \text{ kJ/kg and } h_g = 2724.9 \text{ kJ/kg}$$

Then we can calculate

$$\begin{aligned} h_1 &= (1-x_1)h_f + x_1h_g = (1-0.96316)(561.43) + (0.96316)(2724.9) \\ &= 2645.2 \text{ kJ/kg} \end{aligned}$$

Since our valve is isenthalpic

$$h_2 = h_1 = 2645.2 \text{ kJ/kg}$$

Now going to the saturation pressure table we find

$$P_2 = 50 \text{ kPa}$$

**Problem 2**

A piston-cylinder device contains 0.001 kg of CO<sub>2</sub> at 750 kPa and 1340 K. The device undergoes a polytropic process with polytropic exponent -0.3 or

$$PV^{-0.3} = \text{constant}$$

which decreases the pressure to 550.2 kPa. Determine the boundary work and heat transfer in kJ for this process.

**Solution:** We begin with our template.

Substance Type: Ideal Gas  
 System Type: Closed System  
 Process: Polytropic with  $n=-0.3$   
 Initial State: Fixed  
 Final State: UNKNOWN  
 Q: UNKNOWN

$$W_{sh} = 0$$

$$W_{bnd} = \frac{P_2 V_2 - P_1 V_1}{1 - n}$$

Conserv. of mass:  $m_1 = m_2 = 0.001 \text{ kg}$

1st Law:  $m(u_2 - u_1) = Q - W_{bnd}$

<u>State 1</u>	<u>State 2</u>
$T_1 = 1340 \text{ K}$	$T_2 = 350 \text{ K}$
$P_1 = 750 \text{ kPa}$	$P_2 = 550.2 \text{ kPa}$
$u_1 = 1151.4 \text{ kJ/kg}$	$u_2 = 191.75 \text{ kJ/kg}$
$v_1 = 0.3375 \text{ m}^3/\text{kg}$	$v_2 = 0.1202 \text{ m}^3/\text{kg}$
$V_1 = 3.375 \times 10^{-4} \text{ m}^3$	$V_2 = \mathbf{1.202 \times 10^{-4} \text{ m}^3}$
$m_1 = 0.001 \text{ kg}$	$m_2 = 0.001 \text{ kg}$

*Italicized* values are from air tables or ideal gas relation. **Bold** values are calculated. Approach: At state 1, go to the air tables and get  $u_1$ . Use the ideal gas relation to calculate  $v_1$ . Calculate  $V_1$  from  $v_1$  and  $m_1$ . Use polytropic relation to calculate  $V_2$ . Calculate  $v_2$  from  $V_2$  and  $m_2$ . Calculate  $T_2$  from ideal gas relation. Read  $u_2$  from air tables. Calculate the boundary work from  $PdV$ . Calculate the heat transfer from the 1<sup>st</sup> law.

From the air tables for state 1

$$u_1 = 50,672 \text{ kJ/kgmol} = (50,672)/(44.01) = 1151.4 \text{ kJ/kg}$$

Using the ideal gas law

$$v_1 = \frac{RT_1}{P_1} = \frac{(0.1889)(1340)}{(750)} = 0.3375 \text{ m}^3/\text{kg}$$

Then

$$V_1 = m_1 v_1 = (0.001)(0.3375) = 3.375 \times 10^{-4} \text{ m}^3$$

At state 2 we know the pressure and have a polytropic process so that

$$P_2 V_2^n = P_1 V_1^n \text{ or solving}$$

$$V_2 = V_1 \left( \frac{P_1}{P_2} \right)^{1/n} \text{ or substituting}$$

$$V_2 = (3.375 \times 10^{-4}) \left( \frac{750}{550.2} \right)^{-1/0.3} = 1.202 \times 10^{-4} \text{ m}^3$$

Then

$$v_2 = \frac{V_2}{m_2} = \frac{1.202 \times 10^{-4}}{0.001} = 0.1202 \text{ m}^3$$

We can then determine the temperature at state 2 from

$$T_2 = \frac{P_2 v_2}{R} = \frac{(550.2)(0.1202)}{(0.1889)} = 350 \text{ K}$$

From the air tables for state 2

$$u_2 = 8,439 \text{ kJ/kgmol} = (8,439)/(44.01) = 191.75 \text{ kJ/kg}$$

We can now use our equation for the boundary work

$$W_{\text{bnd}} = \frac{P_2 V_2 - P_1 V_1}{1 - n} = \frac{(550.2)(1.202 \times 10^{-4}) - (750)(3.375 \times 10^{-4})}{1 - (-0.30)} = -0.1439 \text{ kJ}$$

From the 1<sup>st</sup> law we calculate the heat transfer

$$Q = m(u_2 - u_1) + W_{\text{bnd}} = (0.001)(191.75 - 1151.4) + (-0.1439) = -1.1035 \text{ kJ}$$

### **Problem 3**

A proposed new ice maker is composed of two components. The first component is a cooling coil, while the second component is a freezing chamber. Water at 15°C and 100 kPa enters the cooling coil at 0.05 kg/s and exits at 0°C as a 50% - 50% mixture by mass of liquid and solid. Determine the heat transfer rate in kW for the cooling coil.

**Hint:** The enthalpy for subcooled liquid or solid can be calculated from the tables with

$$\text{sub.liq.: } h_1 = h_f(\text{at } T_1) + v_f(\text{at } T_1) \times [P_1 - P_{\text{sat}}(\text{at } T_1)]$$

$$\text{sub.sol.: } h_1 = h_i(\text{at } T_1) + v_i(\text{at } T_1) \times [P_1 - P_{\text{sat}}(\text{at } T_1)]$$



**Solution:** We begin with the cooling coil. Setting up our template,  
 Substance Type: Compressible  
 System Type: Control Volume  
 Device: Heat Device  
 Process: Constant Pressure  
 Inlet State: Fixed  
 Outlet State: UNKNOWN  
 $q = ???$   
 $w_{sh} = 0$   
 1st Law:  $h_2 - h_1 = q$

State 1	State 2
$T_1 = 15^\circ\text{C}$	$T_2 = 0^\circ\text{C}$
$P_1 = 100 \text{ kPa}$	$P_2 = 100 \text{ kPa}$
$h_1 = 63.08 \text{ kJ/kg}$	$h_2 = \mathbf{2645.2 \text{ kJ/kg}}$
Phase: sub. liq.	Phase: 2 phase with $x_2 = 0.50$

*Italicized* values are from steam tables. **Bold** values are calculated.

Approach: With state 1 fixed, we can go to the steam tables and get  $h_f$ ,  $v_f$ , and  $P_{sat}$  at  $15^\circ\text{C}$  and then use the equation in the hint to calculate  $h_1$ . Next we use the constant pressure condition to fix state 2. We calculate the liquid and solid enthalpies using the equation from our hint and then use the quality to calculate  $h_2$ . Use the 1<sup>st</sup> law to calculate the heat transfer rate.

At  $15^\circ\text{C}$  we find

$$h_f = 62.982 \text{ kJ/kg}, v_f = 0.001001 \text{ m}^3/\text{kg} \text{ and } P_{sat} = 1.7057 \text{ kPa}$$

Then using our hint

$$\begin{aligned} h_1 &= h_f(\text{at } T_1) + v_f(\text{at } T_1) \times [P_1 - P_{sat}(\text{at } T_1)] = 62.982 + (0.001001)(100 - 1.7057) \\ &= 63.08 \text{ kJ/kg} \end{aligned}$$

At  $0^\circ\text{C}$  we have

$$h_f = 0.001 \text{ kJ/kg}, v_f = 0.001000 \text{ m}^3/\text{kg} \text{ and } P_{sat} = 0.6117 \text{ kPa}$$

so that

$$\begin{aligned} h_{2,\ell} &= h_f(\text{at } T_2) + v_f(\text{at } T_2) \times [P_2 - P_{sat}(\text{at } T_2)] = 0.001 + (0.001000)(100 - 0.6117) \\ &= 0.1004 \text{ kJ/kg} \end{aligned}$$

and

$$h_i = -333.40 \text{ kJ/kg}, v_i = 0.001091 \text{ m}^3/\text{kg} \text{ and } P_{sat} = 0.61169 \text{ kPa}$$

so that

$$\begin{aligned} h_{2,s} &= h_i(\text{at } T_2) + v_i(\text{at } T_2) \times [P_2 - P_{sat}(\text{at } T_2)] = -333.40 + (0.001091)(100 - 0.61169) \\ &= -333.292 \text{ kJ/kg} \end{aligned}$$

Then

$$h_2 = (0.5)h_{2,\ell} + (0.5)h_{2,s} = (0.5)(0.1004) + (0.5)(-333.292) = -166.596 \text{ kJ/kg}$$

Our 1<sup>st</sup> law then gives

$$\dot{Q} = \dot{m}(h_2 - h_1) = (0.05)(-166.596 - 63.08) = -11.48 \text{ kW}$$