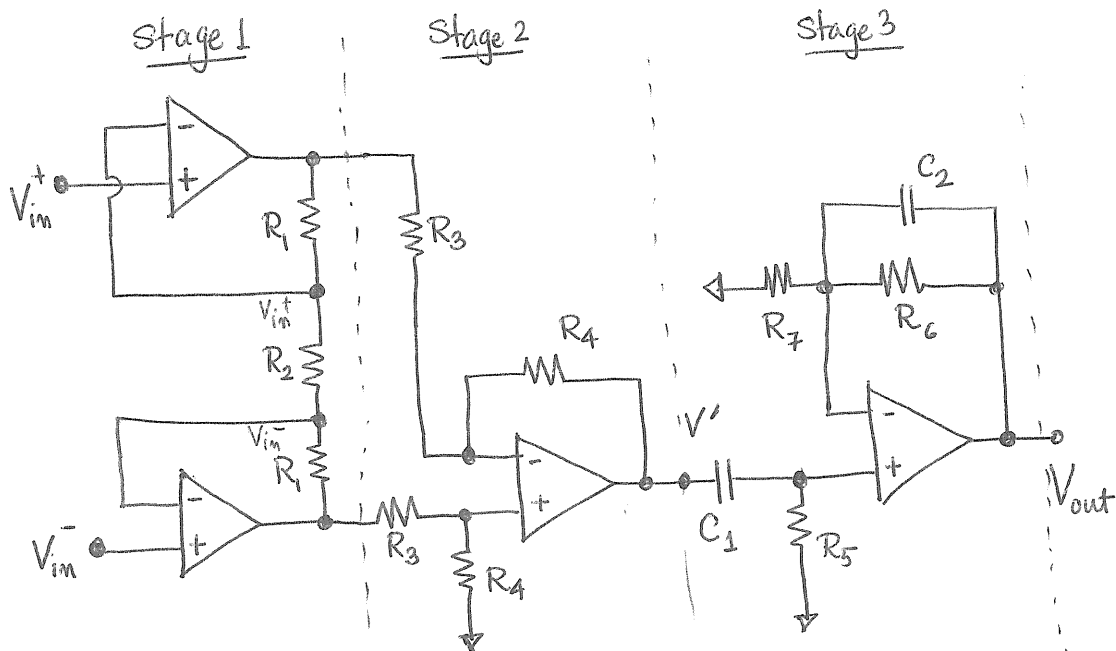


Solution to Exam 1

Problem 1

Part 1



Gain

$$G_1 = \frac{2R_1 + R_2}{R_2}$$

Gain

$$G_2 = -\frac{R_4}{R_3}$$

Transfer function

$$\frac{V_{out}(s)}{V'(s)} = \frac{R_6}{R_7} \frac{sC_1R_5}{(1 + sR_5C_1)(1 + sC_2R_6)}$$

For a ~~gain of 1000~~ derivation of the gain & transfer function see the end of this document or lecture notes.

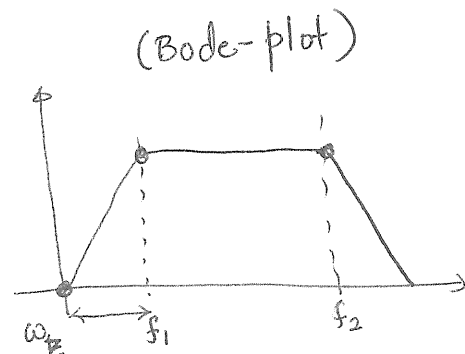
$$\text{Total gain } G = G_1 G_2 \cdot \frac{R_6}{R_7} = \left(\frac{2R_1 + R_2}{R_2}\right) \left(-\frac{R_4}{R_3}\right) \left(\frac{R_6}{R_7}\right)$$

with zeros at $\omega_z = 0$, $\omega_{p1} = 1/R_5C_1$, $\omega_{p2} = 1/R_6C_2$

First satisfy the passband requirements

$$f_1 = \frac{1}{2\pi R_5 C_1} = 0.1 \text{ Hz} \Rightarrow \text{(i)}$$

$$f_2 = \frac{1}{2\pi R_6 C_2} = 10000 \text{ Hz} \quad \text{(ii)}$$



$$R_6 = \frac{1}{2\pi C_2} \times 10^{-4}$$

Choose $C_2 = 10 \text{ pF} \Rightarrow R_6 = 1.6 \text{ M}\Omega$.

Using equation (i)

$$R_5 = \frac{1}{2\pi C_1} \times 10$$

For $C_1 = 1 \mu\text{F} \Rightarrow R_5 = 1.6 \text{ M}\Omega$

To achieve a total gain of 1000

$$G = \left(\frac{2R_1 + R_2}{R_2} \right) \left(-\frac{R_4}{R_3} \right) \left(\frac{R_6}{R_7} \right)$$

$\downarrow \qquad \qquad \downarrow \qquad \qquad \downarrow$
 10 \qquad \qquad 10 \qquad \qquad 10

Choose $R_7 = 160 \text{ k}\Omega$

$R_3 = 10 \text{ k}\Omega$

$R_4 = 100 \text{ k}\Omega$

$R_2 = 10 \text{ k}\Omega$

$R_1 = 45 \text{ k}\Omega$

Part II

First calculate the displacement current

$$i_d = 2\pi f V_{rms} C_b$$

$$\approx 2\pi \cdot 60 \text{ Hz} \cdot 120 \times 0.001 \times 10^{-12}$$

$$\approx 50 \text{ pA}$$

Driven Right-leg system

$$V_{cm} = \frac{R_{RL} i_d}{(1 + 2R_f/R_a)}$$

$$\frac{R_{RL}}{(1 + 2R_f/R_a)} = \frac{2 \times 10^{-3}}{50 \times 10^{-12}} = 4 \times 10^7$$

Choose $R_{RL} \approx 40 \text{ M}\Omega$

and $R_f = 1 \text{ k}\Omega$ $R_a = 100 \text{ k}\Omega$

} You can choose any values for the given requirements

Part III

Interference at the biopotential amplifier due to common mode disturbance

$$V_{im} = V_{cm} \left(\frac{\Delta Z}{Z_{im}} \right)$$

where ΔZ is the difference in impedance of the input electrodes (Z_1, Z_2)

$Z_{im} \rightarrow$ input impedance of the amplifier.

Because the op-amp used for instrumentation amplifier is ideal

$$\Rightarrow Z_{im} = \infty$$

$$\boxed{V_{im} = 0 \text{ V}}$$