

(P4.1) COP = coef. of performance =  $\frac{Q_c}{W_{s,net}}$

Using state numbers of Fig 4.9-4.10. P-H plot will look like Fig 4.10 of pg 151. Use P-H chart pg 653 and table pg 654:

state 2 is satV at  $-40C \rightarrow H_2 = 372 \text{ kJ/kg}$  (chart)

state 3, outlet of the reversible compressor is found by following the isentropic line to  $40C$ , where  $H_3' = 438 \text{ kJ/kg}$ .

state 4 is satL at  $H_4 = 256 \text{ kJ/kg}$  (table)

state 1,  $H_1 = H_4$

$$Q_c = (H_2 - H_1) = 372 - 256 = 116 \text{ kJ/kg}$$

$$W_s = (H_3 - H_2) = 438 - 372 = 66 \text{ kJ/kg}$$

$$\Rightarrow COP = \frac{\dot{Q}_c}{\dot{W}_s} = \frac{116}{66} = 1.76$$

$$Q_c = COP (W_s) = 1.76 (9000 \text{ J/day}) = 16 \text{ kJ/day}$$

(P4.2) Methane,. See Fig 4.9-4.10 pg 150-1. Methane chart pg 651.

$$T_{evap} = -280^\circ F, P = 0.032 \text{ MPa}$$

$$\Rightarrow H_2^{satV} = 339 \text{ Btu/lbm}$$

$$S_2^{satV} = 2.35 \text{ Btu/lb}^\circ F$$

Pressure of 3' isn't given, however, it will be the same as the condenser outlet (P<sub>4</sub>) since the condenser will be considered to be isobaric. State 4 will be satL at 40F, so P<sub>4</sub> = P<sub>3'</sub> = 2 MPa. Follow isentropic line from the compressor inlet state to 2MPa. At P<sub>3'</sub>=2MPa, and S<sub>3'</sub> = 2.35 Btu/lb<sub>m</sub>F, H<sub>3'</sub> = 485 Btu/lbm, and T<sub>3'</sub> = 40F. At the outlet of the condenser, the fluid will be saturated liquid at 2 MPa,

$$T_4 = -160^\circ F, P_4 = 2 \text{ MPa}$$

$$\Rightarrow H_4^{satL} = 218 \text{ Btu/lbm}$$

$$S_4^{satliq} = 1.54 \text{ Btu/lb}^\circ F$$

State	T(°F)	P(MPa)	H(Btu/lb)	S(Btu/lb*°F)
1	-280	0.032	218	
2 Sat'd vap	-280	0.032	339	2.35
3'	<b>40</b>	2	<b>485</b>	2.35
4	-160	2	218	1.54

$$COP = \frac{H_2 - H_1}{H_3' - H_2} = \frac{Q_c}{W_{s,net}} = \frac{H_2 - H_4}{H_3' - H_2} = \frac{339 - 218}{485 - 339}$$

$$\Rightarrow COP = 0.83$$

(P4.3) Rankine Cycle, Fig 4.3 Pg. 143

temperatures  $200^\circ C$  &  $99.6^\circ C$ , Sat vapor from Turbine outlet can be found in the sat Pressure table p642.

## Chapter 4 Practice Problems

The turbine is assumed to be adiabatic and reversible since no other specifications are given. The inlet state will then have the same entropy as the outlet. Since the boiler/superheater outlet is to operate at  $T_3 = 200\text{ C}$ , and  $S_3 = 7.3592$ , we must hunt in the superheated tables to find this combination. This will occur between 0.2 and 0.3 MPa. Interpolating, the value of H can be found. Values are tabulated below:

State	T(°C)	P(MPa)	H(kJ/kg)	S(kJ/kg·K)	V(m <sup>3</sup> /kg)
4' sat vap	99.6	0.098	2675	7.359	
5 sat liq.	99.6	0.098	417	1.3028	0.001043
	3	200	2867	7.3592	
	6		417.18		

$$W'_{S,turbine} = (H'_4 - H_3) = 2675 - 2867 = -192\text{ kJ / kg}$$

$$\Delta H_{pump} = W_{S,pump} = \int VdP = V\Delta P$$

$$\Rightarrow \Delta H_{pump} = \frac{1043\text{ cm}^3 * (0.271 - 0.098)}{\text{kg}} * \frac{1\text{ J}}{\text{cm}^3 * \text{MPa}} * \frac{\text{kJ}}{10^3\text{ J}}$$

$$\Rightarrow \Delta H_{pump} = 0.180\text{ kJ / kg}.$$

$$\Rightarrow W'_{S,net} = -192 + 0.180 = -191.82\text{ kJ / kg}$$

$$\& \eta = \frac{-W'_{S,net}}{Q_{boiler}} = \frac{-(-191.82)}{(H_3 - H_6)} = \frac{-(-191.82)}{(2867 - H_6)}$$

$$\Rightarrow H_6 = 417 + 0.18 = 417.18\text{ kJ / kg}$$

$$\Rightarrow \eta = \frac{-(-191.82)}{(2867 - 417.18)} = 0.0783$$

$$\Rightarrow \eta = 7.83\%$$